

Intelligent Control for Electric-Vertical Take Off and Landing (e-VTOL) Aircraft

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CASI AERO 2023, November 14-16, 2023

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- 5 Momentum Analysis of e-VTOL Aircraft in Transition
- 6 Development of e-VTOL Flight Simulator
- 7 Conclusion



Figure 1: BETA Aircraft ALIA-250 e-VTOL in forward flight [1]

1. Motivation

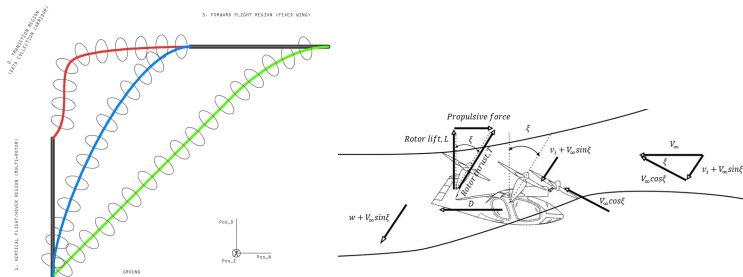
- In recent years there has been a growing interest in the possibilities of aerial mobility using Electric Vertical Takeoff and Landing, or e-VTOL aircraft. These vehicles combines feature from Fixed-Wing and Rotor-wing vehicles.
- e-VTOL aircraft combine the maneuvering capabilities of multi-rotors with the greater range and endurance as well as flight speeds of fixed-wing aircraft
- We aim to develop a customized e-VTOL aircraft flight simulator built from existing obsolete fixed-wing simulator hardware. Further, our mission is to connect this modified flight simulator to research on aspects of operation or control of e-VTOL aircraft.

2. Introduction

- Recent advancement in the electric-Vertical Take off and Landing (e-VTOL) aircraft sector brings the question of whether the technology will be fully autonomous, or remotely piloted, or with actual crew onboard.
- There are inherent challenges in operation of such aircraft configurations:
 - Propellers wake interactions.
 - Lack of flight test data.
 - Non-linearities in thrust, drag, and actuation.
- One of the flight regimes requiring further investigation was the transition from hovering to forward flight.
- In this regime, the vehicle moves from a helicopter hover in still air and gains forward speed to transition to fixed wing

2. Introduction

- An example of transition regime is shown in the diagram below:



(a) Different transition regimes for e-VTOL

(b) Velocities and Force Distribution on e-VTOL during transition

Figure 2: e-VTOL Transition: Tilt-rotor example

2. Introduction

- e-VTOL aircraft, due to their hybrid configuration, need rethinking.
- They exhibit aerodynamics interaction between propellers, fuselage, and operate in regimes shared between a helicopter and fixed-wing aircraft.
- Some of the common challenges for e-VTOL vehicles are:
 - Rotor-fuselage and rotor-wings interactions.
 - Lack of empirical data from flight tests.
 - Challenging control characteristics:
 - Control degradation after rotor failures;
 - transition region between fixed-wing and helicopter motion;
 - rotor tilting mechanism, to mention a few.

3. Literature Distribution

3.1 Intelligent Control for Transition Flight

Many of literature rely on model-based methods and have shortcomings if the models are not accurately representative. Making our case for Intelligent Control for transition flight promising.

- 250 papers surveyed.
- 28 papers of high relevance.
- divided into categories below:

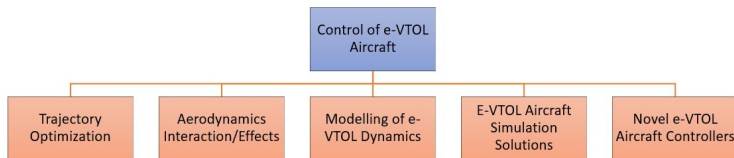


Figure 3: Distribution of Literature for e-VTOL Control [2], [3], [4], [5], [6], [7], [8]

4. Thrust and Lift requirements for e-VTOL

4.1 Example: Tiltrotor e-VTOL Aircraft

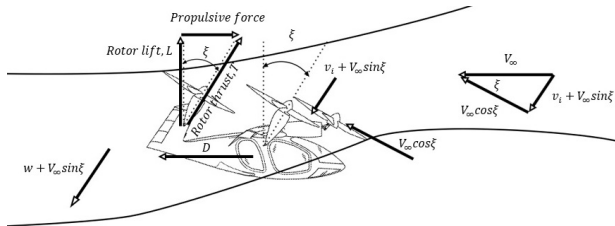


Figure 3: Velocity and Forces on Tilt-rotor e-VTOL [9]

Specifications and flight condition:

Table 1: Specifications for Example Tilt-rotor e-VTOL Aircraft [1]

m (kg)	S (m^2)	b (m)	\bar{c} (m)	CL_{α_0} (NACA - 2412)	ρ ($\frac{kg}{m^3}$)	W (N)
2000	24	15	1.6	0.20	1.225	20000

4.1 Example: Tiltrotor e-VTOL Aircraft

$$L_{wing} = \frac{1}{2} \rho V_{\infty}^2 S C_{L\alpha=0} \quad (1)$$

$$T_{vertical} = W \cos(\xi) \quad (2)$$

$$T_{horizontal} = W \sin(\xi) \quad (3)$$

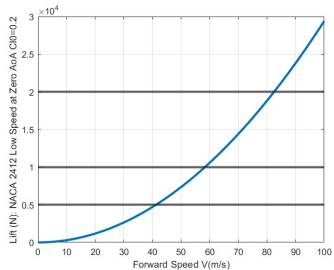
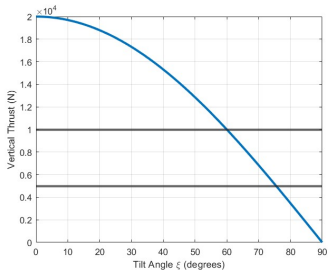


Figure 4: Propeller Lift and Wing Lift

To sustain the weight, we need about $V = 85\text{m/s}$.
 Assuming forward acceleration $a = 9.81 \frac{\text{m}}{\text{s}^2}$ and no drag. to get to 85 m/s it will take 9 seconds approximately. Meaning:

$$V = at + V_0 = 9.81t \quad (4)$$

Lift equation will be modified with respect to time:

$$L_{\text{wing}} = \frac{1}{2}\rho(9.81t)^2 SC_{L\alpha=0} \quad (5)$$

Similarly, we assume 10 seconds to deploy to fully horizontal e-VTOL configuration, this gives a tilting rate of 9 degrees/sec, giving:

$$\xi = \dot{\xi}t = 9t \quad (6)$$

Vertical thrust will be modified with respect to time as:

$$T_{\text{vertical}} = W\cos(\xi t) = W\cos(9t) \quad (7)$$



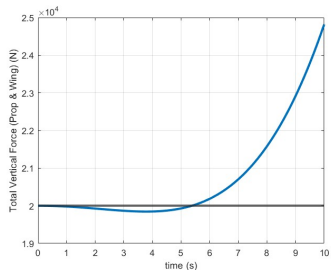
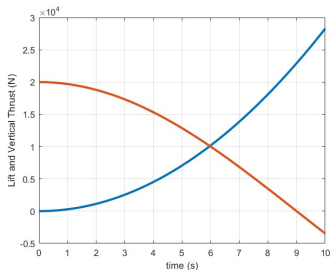
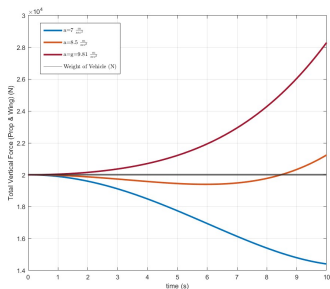


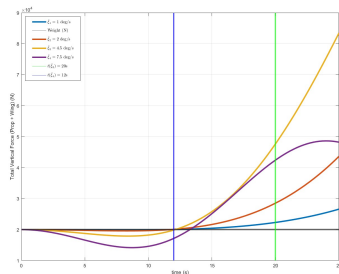
Figure 5: Wing Lift and Vertical Thrust Combined Effects

Finally, the combined effort will be given:

$$L_{total} = T_{vertical} + L_{wing}$$



(a) L_{total} for various accelerations:
10s transition time



(b) L_{total} for various tilting rates $\dot{\xi}$

Figure 5: Forward Acceleration Effect and Tilt-rate Effects on Lift

- Following conclusions can be drawn from above investigation:
 - Forward acceleration impacts wing lift.
 - Tilting rate impact loss of lift for combined propeller + wing.
 - Nonlinear effects.

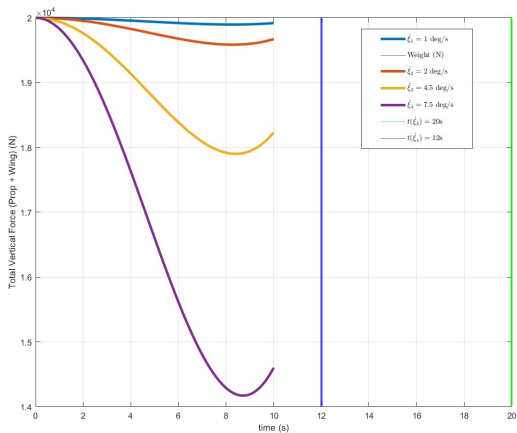


Figure 6: Detailed View L_{total} for various tilting rates $\dot{\xi}$

5. Momentum Analysis of e-VTOL Aircraft in Transition

5.1 Induced velocity v_i in Forward Flight

From momentum studies for helicopters [9] we have:

$$T = 2\dot{m}v_i = 2(\rho AU)v_i \quad (9)$$

Or:

$$T = 2\rho Av_i \sqrt{(V_\infty \cos\xi)^2 + (V_\infty \sin\xi + v_i)^2} \quad (10)$$

We re-arrange in terms of hover condition, $T = 2\rho Av_h^2$

$$v_i = \frac{v_h^2}{\sqrt{(V_\infty \cos\xi)^2 + (V_\infty \sin\xi + v_i)^2}} \quad (11)$$

Define following parameters:

In-flow ratio λ and tip-speed ratio (advance ratio) μ :

$$\lambda = \frac{V_\infty \sin\xi + v_i}{\Omega R} \quad \text{and} \quad \mu = \frac{V_\infty \cos\xi}{\Omega R} \quad (12)$$

Therefore arriving at

$$\lambda = \frac{V_{\infty} \sin \xi}{\Omega R} + \frac{v_i}{\Omega R} = \mu \tan \xi + \lambda_i \quad (13)$$

These equations modify the thrust equation shown earlier in terms of in-flow ratios:

$$\lambda_i = \frac{\lambda_h^2}{\sqrt{\lambda^2 + \mu^2}} \quad (14)$$

Where we have hover inflow ratio $\lambda_i = \sqrt{C_T/2}$. The solution for in-flow ratio will be:

$$\lambda = \mu \tan \xi + \frac{C_T}{2\sqrt{\lambda^2 + \mu^2}} \quad (15)$$

Which can be solved for λ numerically. Results for different disk Angle of Attack (or tilt angle in case of e-VTOL aircraft) are shown in next page:



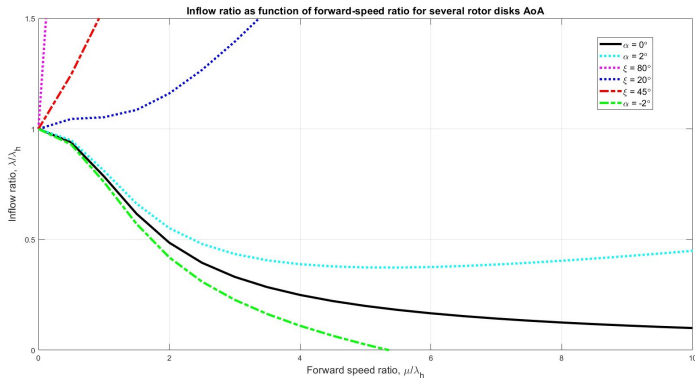


Figure 7: Inflow ratio vs. Forward speed ratio: Helicopter vs. Tilt-rotor e-VTOL

- Nonentities of induced in-flow ratio resulting in non-linearity of thrust distribution.
- strong dependence on AoA or tilt angle.

5.2 Intelligent Control Based on Learning from Data

We showed two examples of nonentities in developing a model for our e-VTOL vehicle. There are additional factors that can cause additional modelling complexities for the e-VTOL configuration:

- Wing Drag: Drag Coefficient C_d can vary significantly from nominal value due to multiple propellers on-wing.
- interference effects between propellers, wing, fuselage.
- Tilting mechanism, it's acceleration $\ddot{\xi}$ will result in counter pitch-up moment of the e-VTOL vehicle air frame, introducing additional AoA to the inflow equation.
- Overlap of in-flows: due to propellers proximity to each other.

This is where we believe we would see a promising data-driven approach that can demonstrate safe close-loop performance using learning based control.



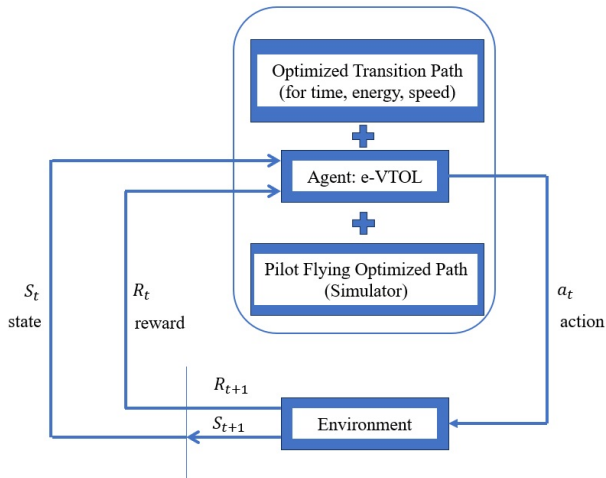


Figure 8: Intelligent Control learning from fusion of data and model

6. Development of e-VTOL Flight Simulator

As a stepping stone towards our research, two important milestones were to happen to provide us assurance that our FSC Simulator can be a suitable platform:

- Be able to use MATLAB/Simulink for visualization of aircraft states;
- re-activate the FSC Simulator to make it suitable for e-VTOL aircraft.

For the first step, I focused on development of basic aircraft visualization on MATLAB/Simulink, and the Research Civil Aircraft Model (RCAM a twin-engine Fixed-Wing transport category aircraft [10] [11]) plus MATLAB/Simulink Aerospace Blockset for visualization of aircraft states was constructed.



6. Development of e-VTOL Flight Simulator

- Cost-effective: We took elements of the existing fixed-wing setup and built an e-VTOL type simulator around it.
- Uses X-Plane for visualization, Air Manager for instrumentation, Matlab/Simulink for research.
- Built to resemble modern e-VTOL cockpit.

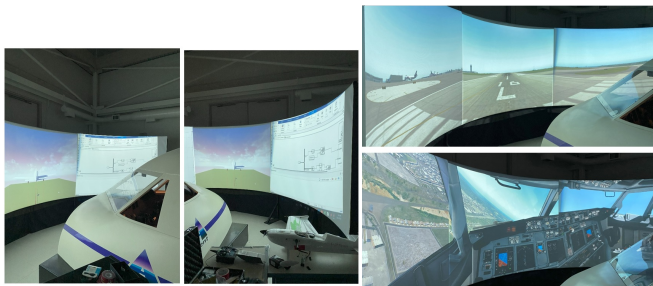


Figure 9: FSC e-VTOL Simulator Setup based on RCAM

6. Development of e-VTOL Flight Simulator

6.1 Simulator Block Diagram

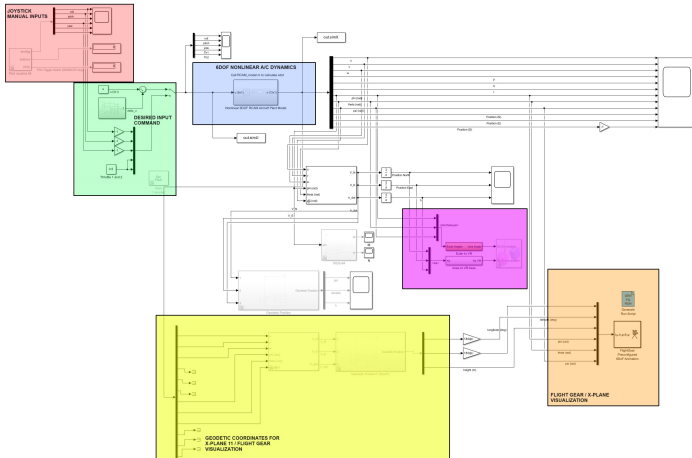


Figure 10: Intelligent Control Learning from fusion of data and model

6. Development of e-VTOL Flight Simulator

6.2 Simulator System Architecture

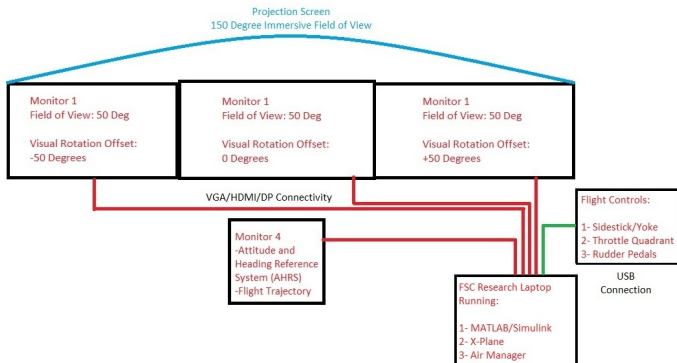


Figure 11: Architecture for Proposed e-VTOL Simulator based on FSC Simulator

6. Development of e-VTOL Flight Simulator

6.3 Open Loop Simulation

With equal thrust command on Th_1 and Th_2 and initial cruise velocity of $u_0 = 85 \frac{m}{s}$ we have following open loop response for $t_{sim} = 180s$:

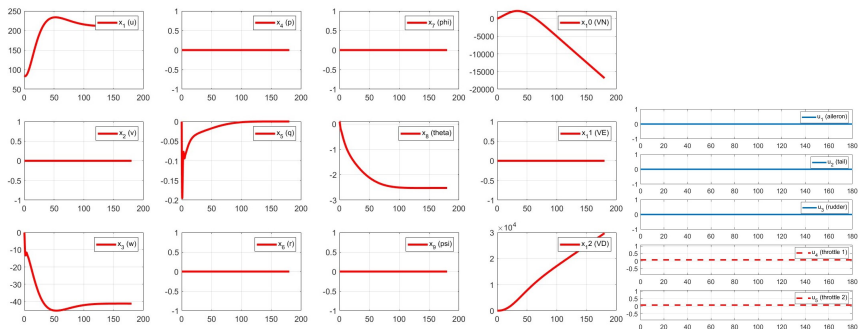


Figure 12: Open Loop Response to equal throttle command

6. Development of e-VTOL Flight Simulator

6.4 Open Loop Simulation

Simulating a roll and pitch command by pilot between $t_0 = 0s$ and $t_0 = 40s$ we have following open loop response will be:

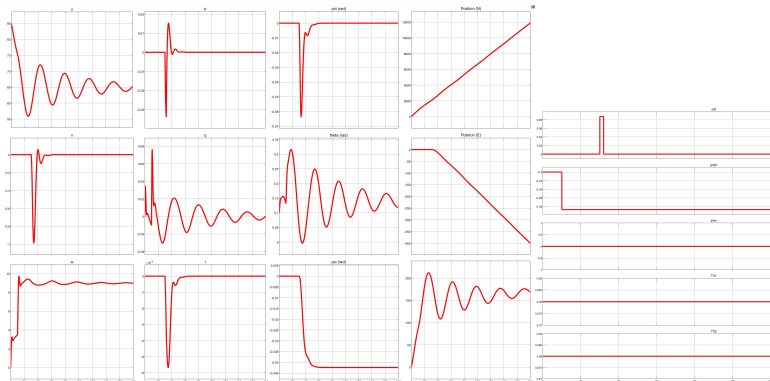


Figure 13: Open Loop Response to equal throttle command

7. Conclusion

- Nonlinear RCAM Simulator implemented.
- Phase 1: FSC Simulator Modification.
- Learning-Based Intelligent Control research.
- Problem of Transition Flight of e-VTOL identified.
- Upcoming:
 - Phase 2: Preparation of e-VTOL Flight Simulator.
 - Refining problem description.
 - Learning Based Intelligent Control vs. existing controllers.



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